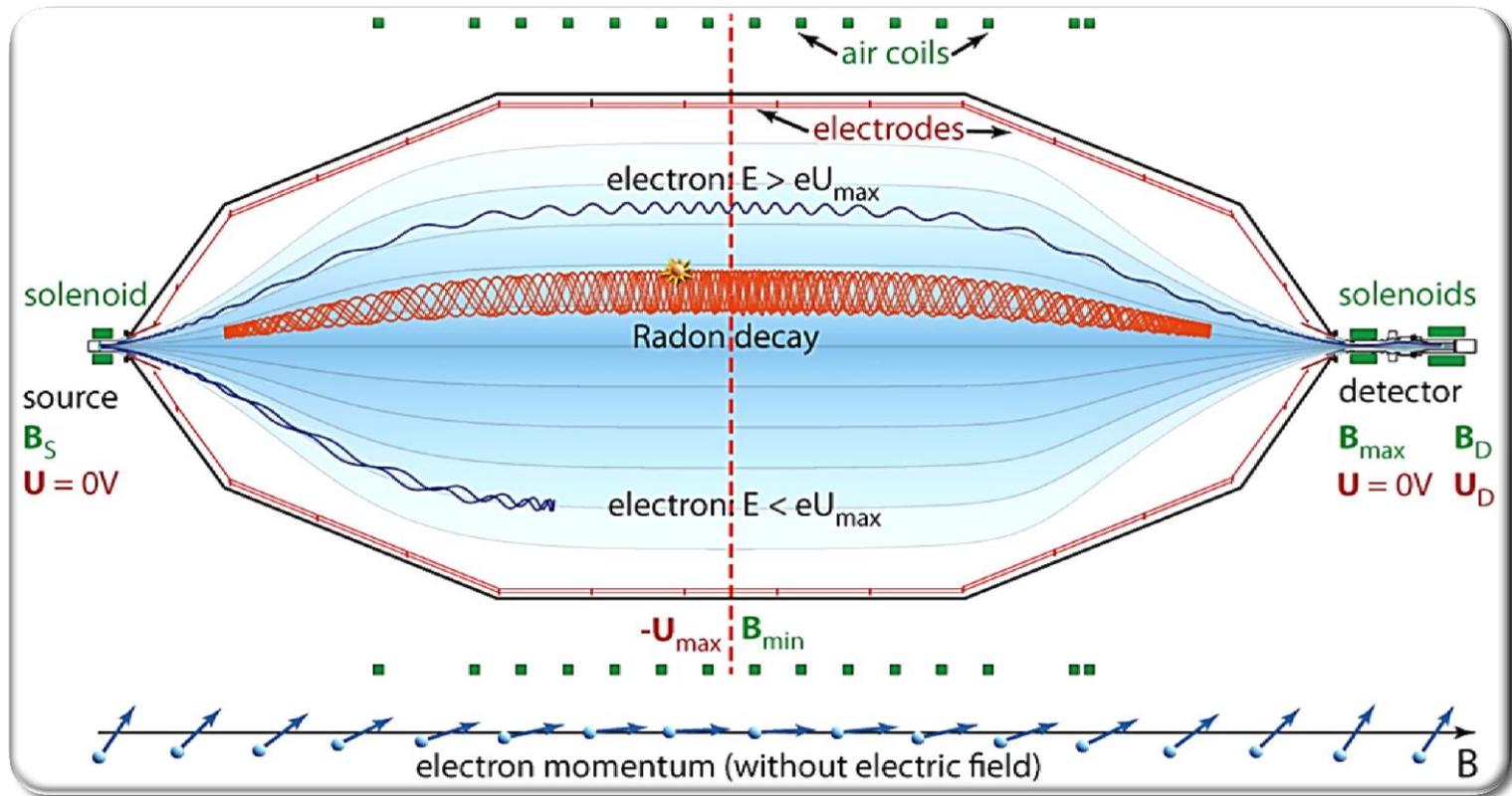


The KATRIN Main Spectrometer

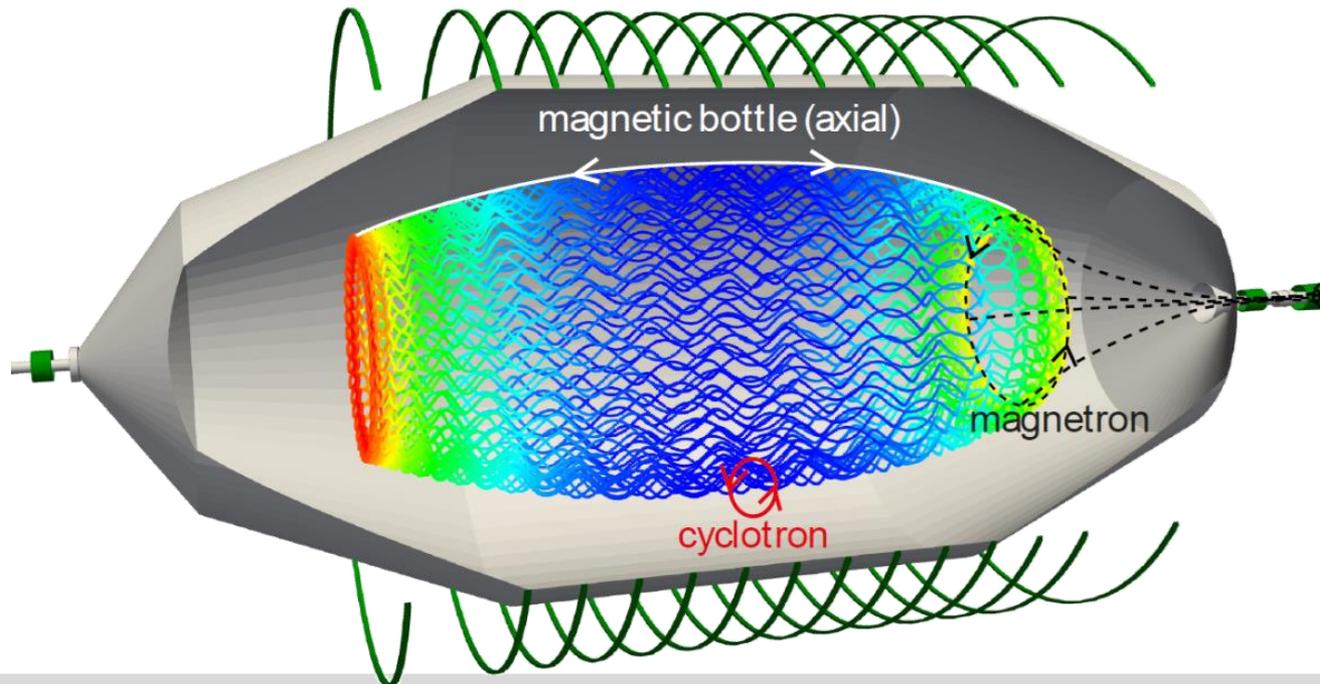
- **MAC-E filter: high pass filter for e^-**
 - magnetic adiabatic collimation ($B_{\min} = 0.3 \text{ mT}$, $B_{\max} = 6 \text{ T}$)
 - electrostatic filter ($-U_{\max} = -18.6 \text{ kV}$)
- **Detector:**
 - counts electrons that passed the filter



Radon background in the Main Spectrometer

■ Challenges:

- neutrino mass measurement requires **low background rates (< 10 mcps)**
- **radon is emanated inside** the spectrometer
- **radon decays** can produce **electrons**, which are **captured** in E, B fields
- **primary electrons** ionize residual gas, producing **secondary electrons**
- **increased background** rate for up to **several hours**



Radon background in the Main Spectrometer

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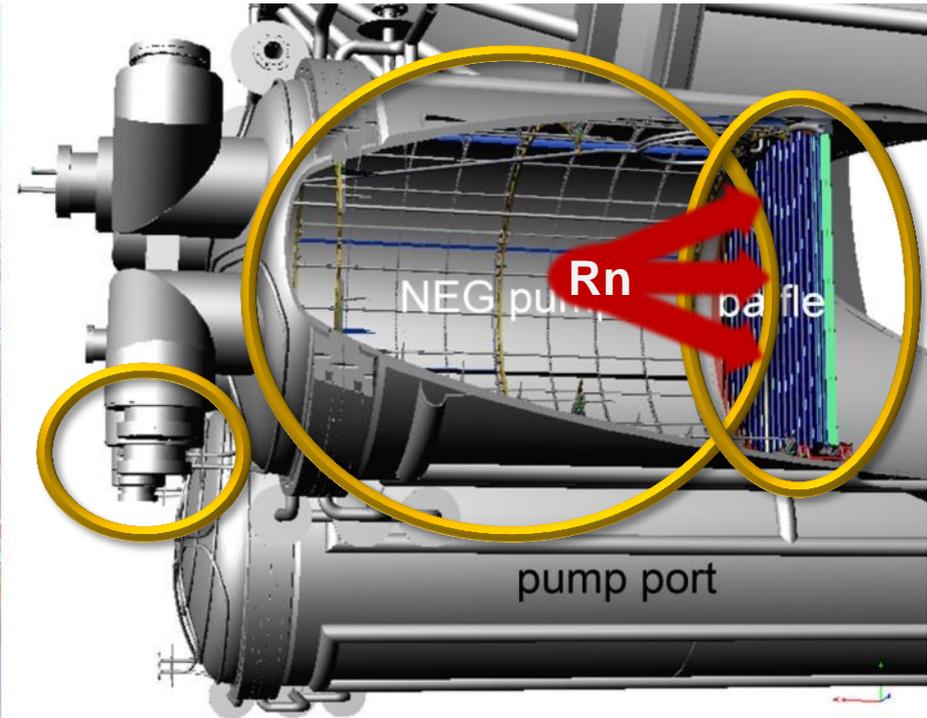
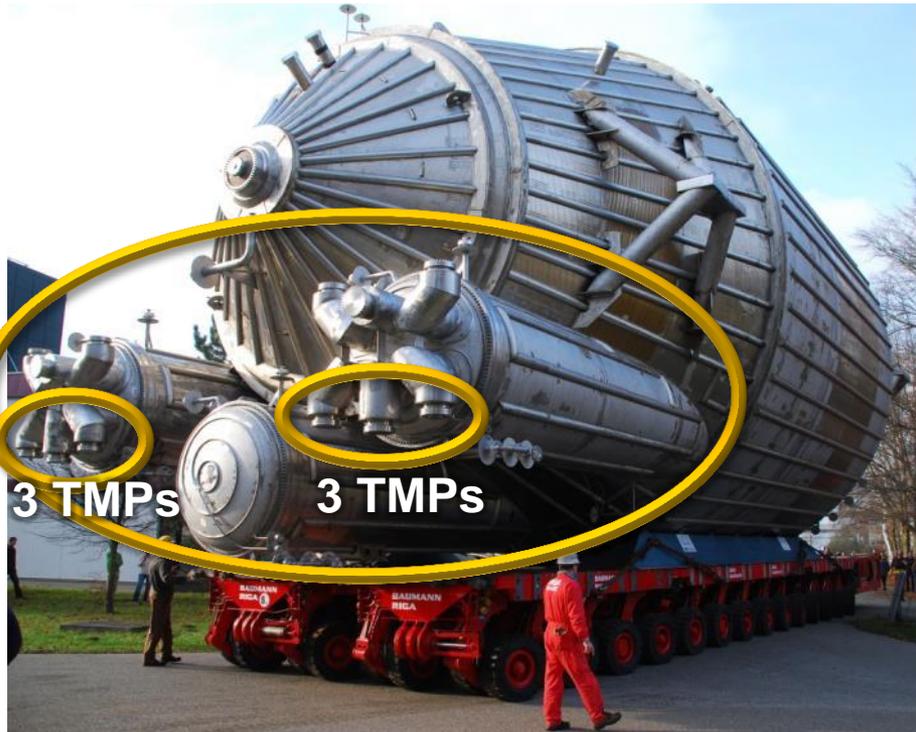
■ Goals:

- **prevent Rn from entering** the Main Spectrometer volume (**→ LN₂ baffle**)
- **remove Rn quickly** from the main volume, before it decays (**→ LN₂ baffle**)

■ Vacuum Simulation:

- determine the **Rn decay rates** for different **pumping speeds**
- uses TPMC code **MolFlow+** for ultra-high vacuum simulation
- influence of **half-life** of different Rn isotopes ?

Main Spectrometer vacuum system



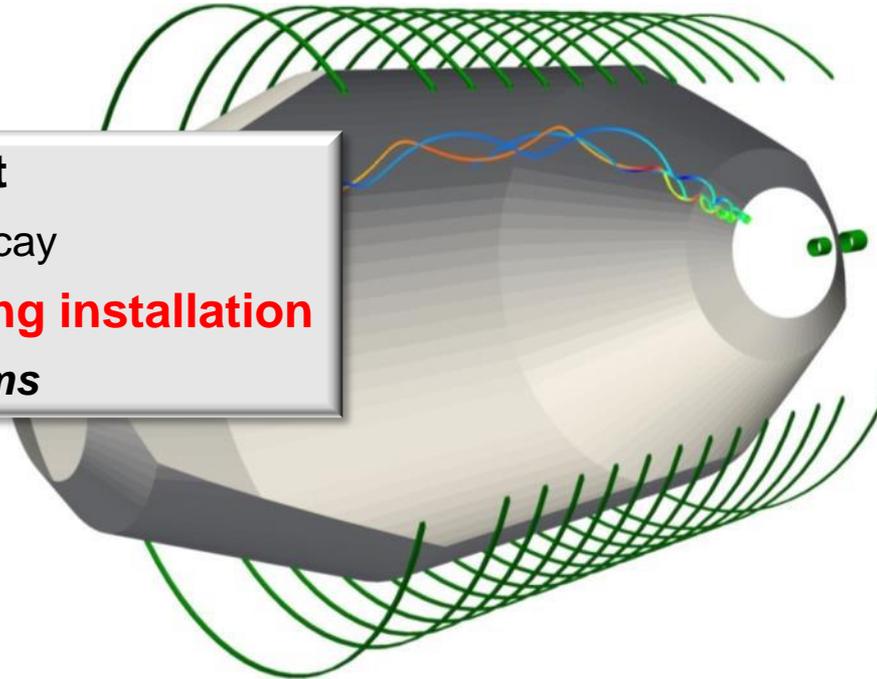
- stainless steel vessel (316LN): **23 m long, 10 m diameter**
- vacuum: **10^{-11} - 10^{-10} mbar**
- **6 turbo-molecular pumps** (Leybold MAG-W 2800): 10 000 ℓ/s (H_2)
- ~~3~~ **NEG-pumps** (~~3000~~ m SAES St707 getter strips): ~~$\sim 10^6 \ell/s$~~ (H_2) **250 000 ℓ/s**
- **3 cryogenic LN_2 Cu-baffles** against radon: $\leq 180\,000 \ell/s$ (Rn)

Possible radon sources

U-238 decay chain

$^{222}\text{Rn} : t_{1/2} = 3.8\text{d}$

- quickly pumped out
 - almost no direct decay
- **long exposure during installation**
 - *see talk by F. Harms*



magnetic & electrostatic fields
do not shield the fluxtube
against **neutral unstable** atoms

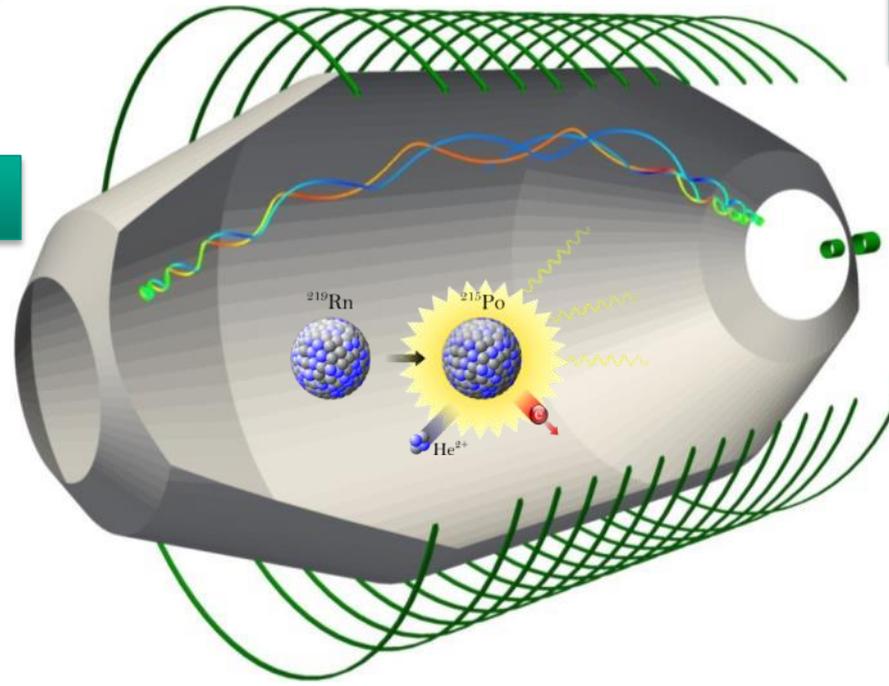
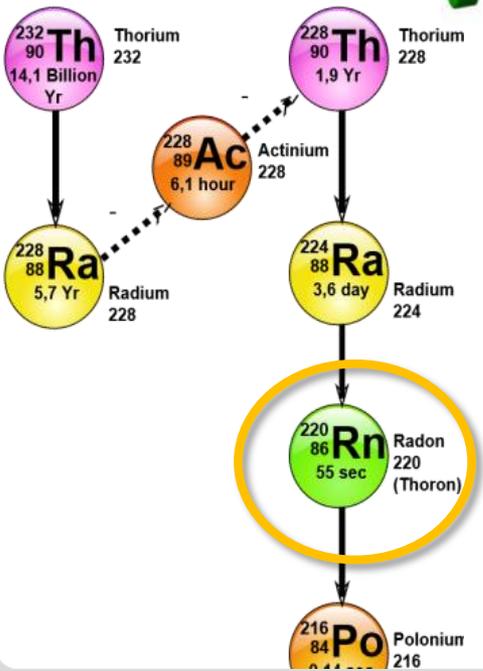
Possible radon sources

U-238 decay chain

$$^{222}\text{Rn} : t_{1/2} = 3.8\text{d}$$

Th-232 decay chain

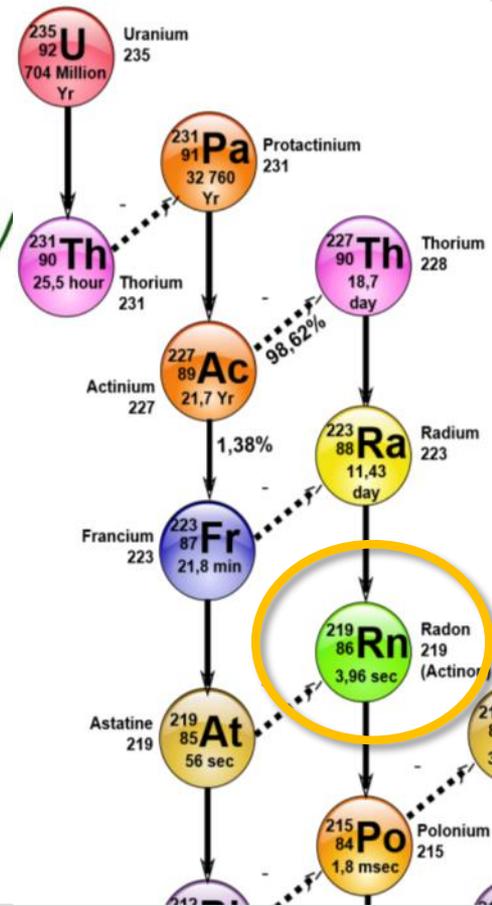
$$^{220}\text{Rn} : t_{1/2} = 55.6\text{s}$$



magnetic & electrostatic fields
do not shield the fluxtube
against **neutral unstable** atoms

U-235 decay chain

$$^{219}\text{Rn} : t_{1/2} = 3.9\text{s}$$



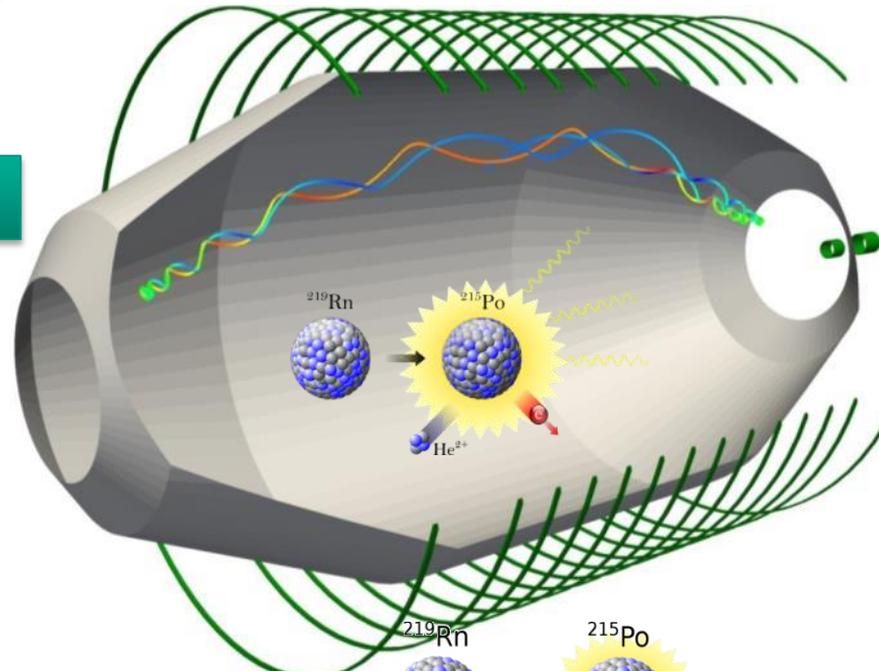
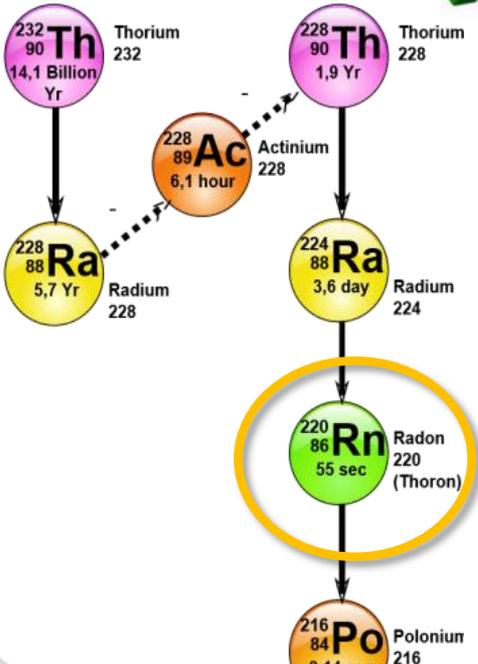
Possible radon sources

U-238 decay chain

$^{222}\text{Rn} : t_{1/2} = 3.8\text{d}$

Th-232 decay chain

$^{220}\text{Rn} : t_{1/2} = 55.6\text{s}$

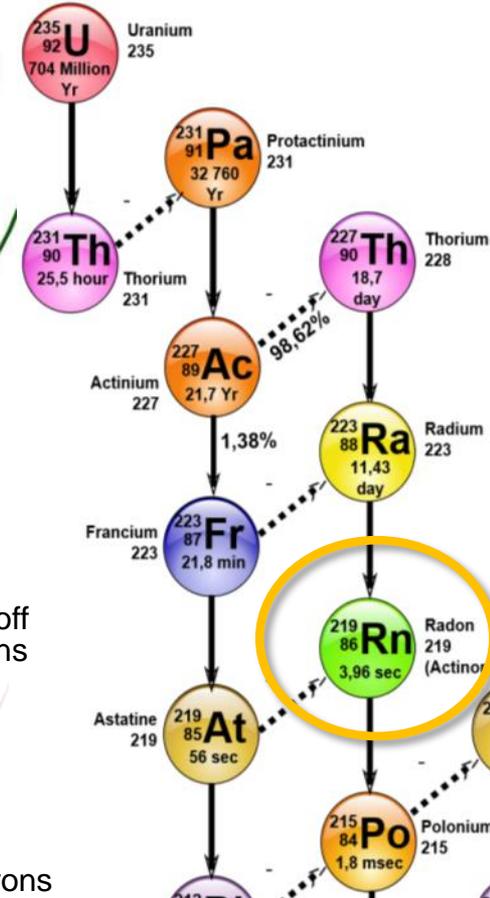


electrons:
eV – 200 keV



U-235 decay chain

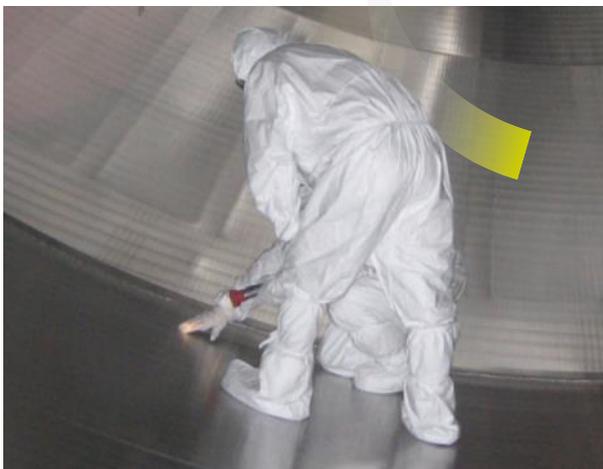
$^{219}\text{Rn} : t_{1/2} = 3.9\text{s}$



Possible radon sources

weld seams

^{220}Rn emanation
(in main volume)

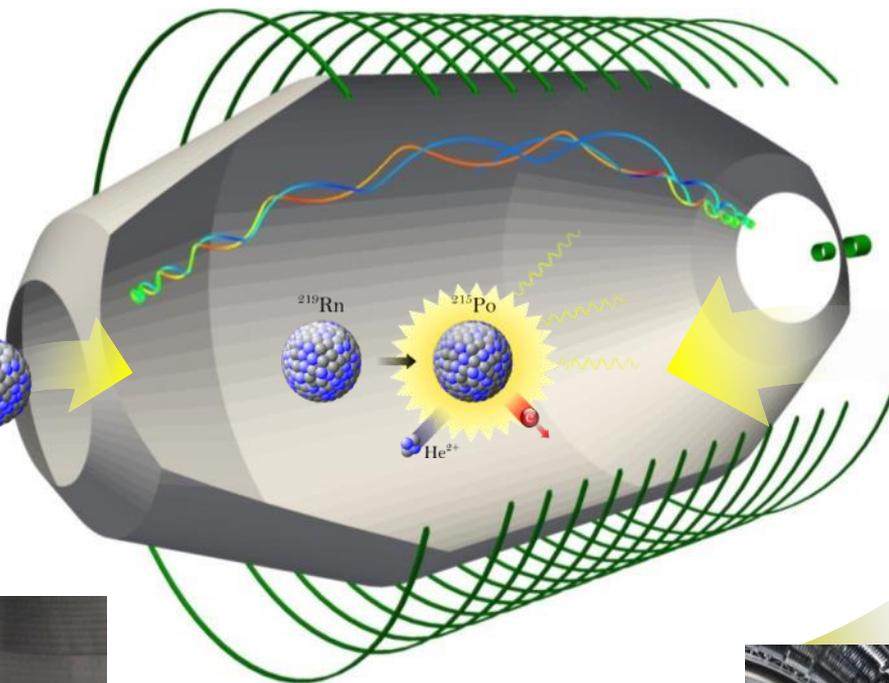
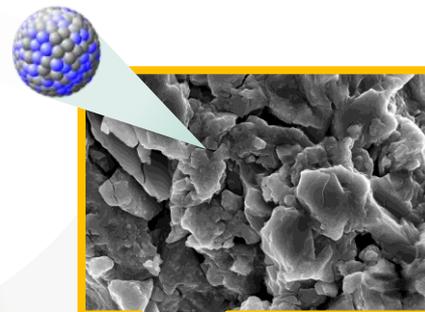


1222 m² 316 LN

3000 m NEG strips

NEG pumps

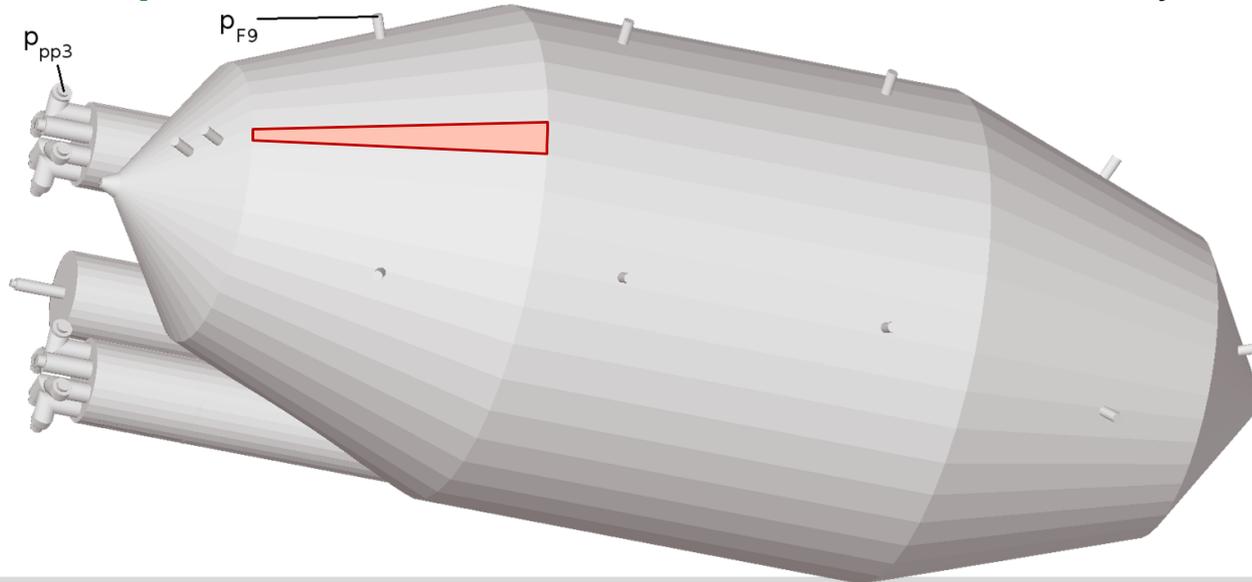
^{219}Rn emanation
(behind baffle)



Simulation of the Main Spectrometer

- **MolFlow+**: Test Particle Monte Carlo code
 - **stable particles**, no radioactive decay
 - **adsorbed particles** stay on a surface indefinitely (**exit condition**)
 - **adsorption** on a surface element is controlled by the **sticking coefficient α**
- **Radon gas**:
 - **radioactive decay** → decay in volume (**second exit condition needed**)
 - **finite sojourn time** on surface
 - **re-desorption** similar to diffuse **reflection** with time delay

$$\tau_{\text{des}} = \tau_0 \cdot \exp(\Delta H_{\text{des}}/R \cdot T_B)$$



Calculation of the Rn decay rate

Rn activity in spectrometer volume

$$A_{Rn} = \lambda_{Rn} \cdot N_{Rn}$$

$$\frac{dN_{Rn}}{dt} = Q_{Rn} - A_{Rn} - \frac{N_{Rn}}{V} \cdot S_{eff} = 0$$

$$A_{Rn} = Q_{Rn} \frac{\lambda_{Rn}}{\lambda_{Rn} + S_{eff}/V}$$

N_{Rn} = Rn atoms in spectrometer

Q_{Rn} = **emanation rate** (desorption)

A_{Rn} = $N_{Rn} \cdot \lambda_{Rn}$ = **activity in spectrometer**

$T_{1/2}$ = radioactive half-life

λ_{Rn} = $\ln(2)/T_{1/2}$ = decay rate

V = spectrometer volume (1240 m³)

S_{eff} = **effective pumping speed for Rn**

effective pumping speed S_{eff}

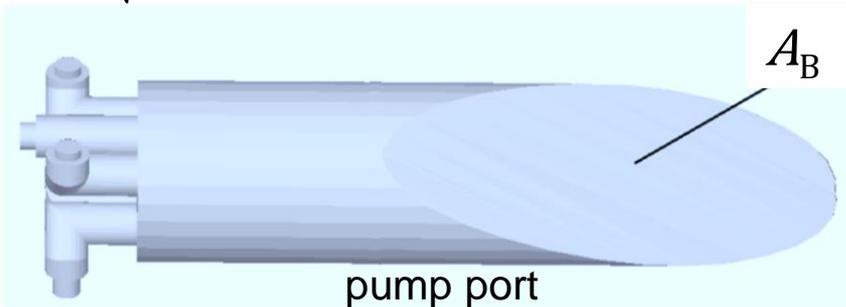
$$S_{eff} = \frac{1}{4} \cdot \bar{c} \cdot A_B \cdot \alpha_{eff}$$

(simulation of pumping surface)

α_{eff} = **effective sticking coefficient**

A_B = opening area of the baffle

$\bar{c} = \sqrt{\frac{8 \cdot k_B \cdot T}{\pi \cdot M}}$ = mean particle speed



Effective sticking coefficient for Rn

- probability for **(permanent) adsorption per hit: α**

Effective sticking coefficient for Rn

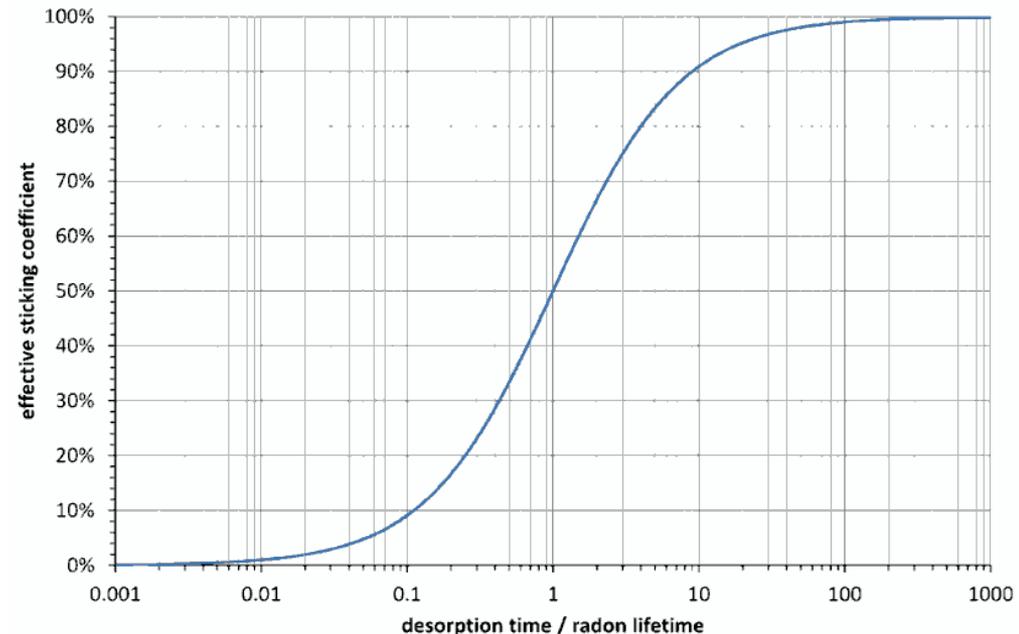
- probability for **hitting the baffle, and decay**: α_{eff}
- probability for **not decaying**: $\exp(-t/\tau_{\text{Rn}})$
- probability for **not desorbing**: $\exp(-t/\tau_{\text{des}})$
- **decay rate at time t**:

$$\frac{dN}{dt} = \lambda_{\text{Rn}} \cdot N(t) = \frac{N_0}{\tau_{\text{Rn}}} \cdot \exp\left(-t \cdot \left(\frac{1}{\tau_{\text{Rn}}} + \frac{1}{\tau_{\text{des}}}\right)\right)$$

- **integration from $t=0$ to infinity**:

$$\alpha_{\text{eff}} = \alpha_0 \cdot \frac{1}{1 + \tau_{\text{Rn}}/\tau_{\text{des}}}$$

(here: $\alpha_0 = 1$)



MolFlow+ simulation of radon decays

■ Standard MolFlow+ simulation:

- use **effective sticking coefficient** for simulating **pumping speed** S_{eff}
- apply simple **models for activity and transmission**
- works for simple geometries
- difficult for complex setups

$$\alpha_{\text{eff}} = \alpha_0 \cdot \frac{1}{1 + \tau_{\text{Rn}}/\tau_{\text{des}}}$$

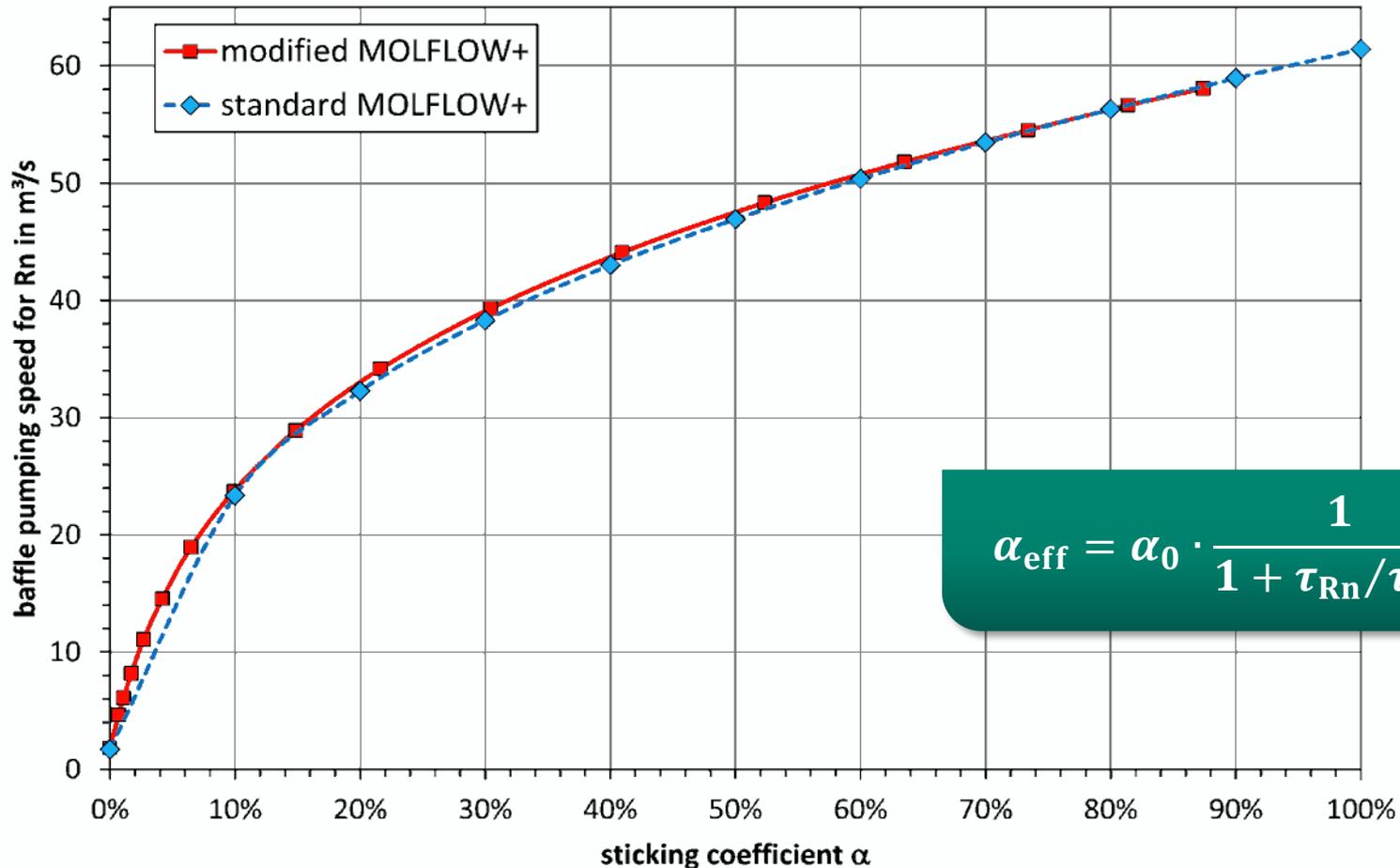
$$A_{\text{Rn}} = Q_{\text{Rn}} \cdot \frac{\lambda_{\text{Rn}}}{\lambda_{\text{Rn}} + S_{\text{eff}}/V}$$

■ Extended version of Molflow+:

- individual **sojourn time** τ_{des} for each surface element ($\alpha_0 > 0$)
- **life-time** τ_{Rn} assigned to particles
 - **decay while adsorbed** on surface: (**1st exit condition** = „pumped out“)
 - **decay in flight:** (**2nd exit condition**)
 - **3D coordinates saved**, if particle decays in flight → **decay map**
- works for arbitrary geometries, re-desorptions, and pumping configurations

Simulation examples: pumping speed

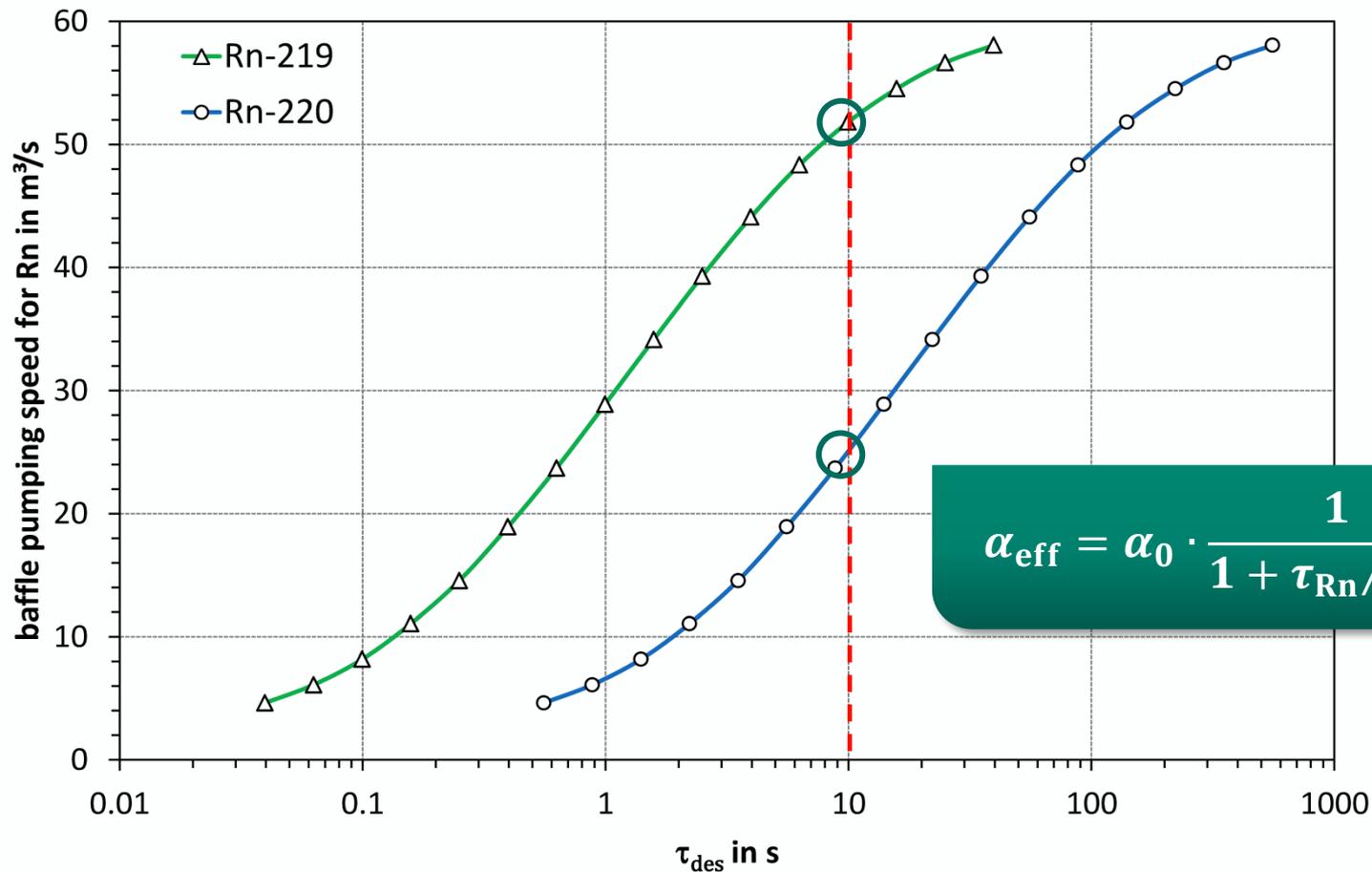
- Effective pumping speed for **6 TMPs**: **3 400 ℓ/s**
- Effective pumping speed for **3 baffles**: **~180 000 ℓ/s** (max)



$$\alpha_{\text{eff}} = \alpha_0 \cdot \frac{1}{1 + \tau_{\text{Rn}}/\tau_{\text{des}}}$$

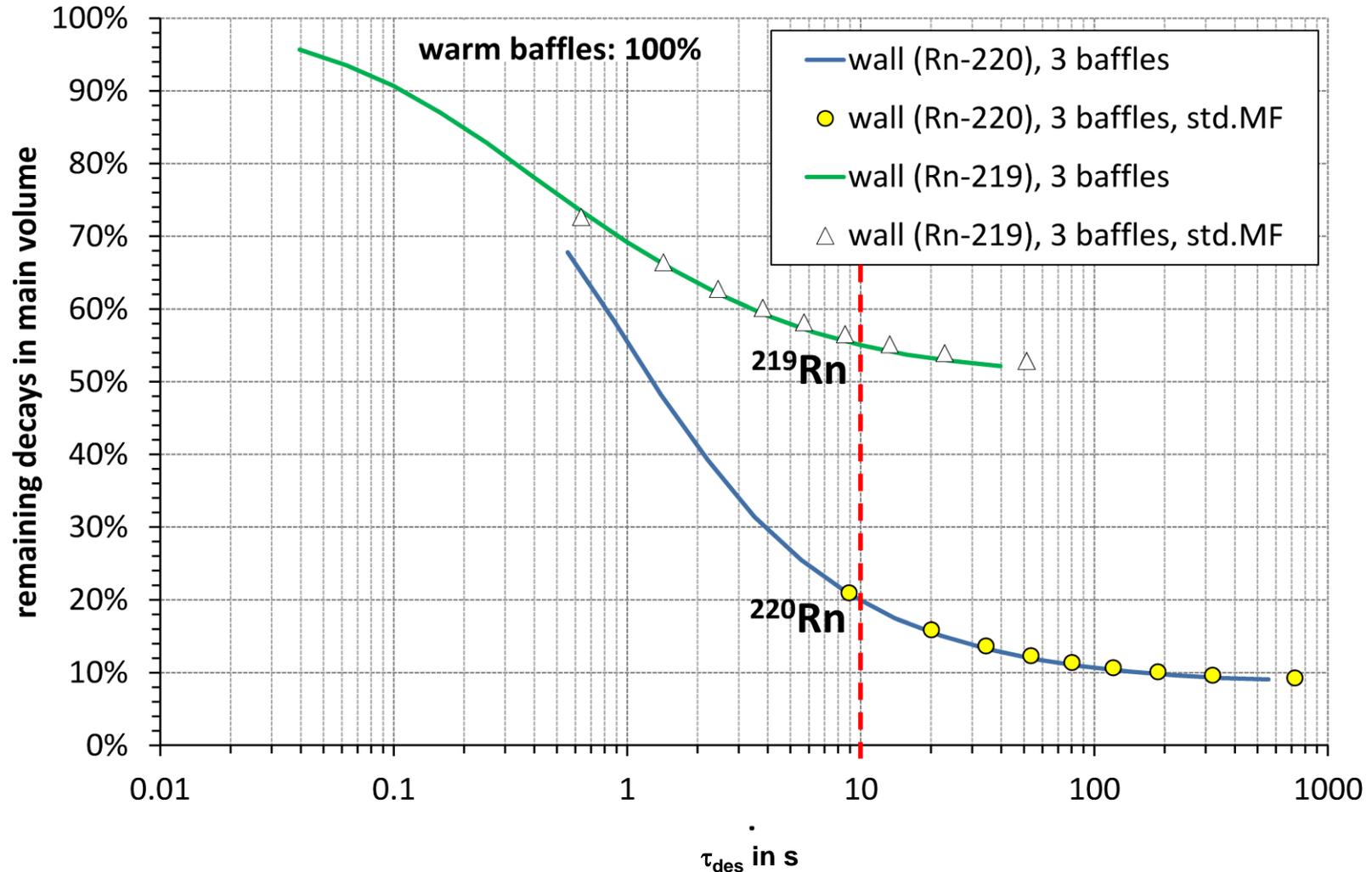
Simulation examples: pumping speed

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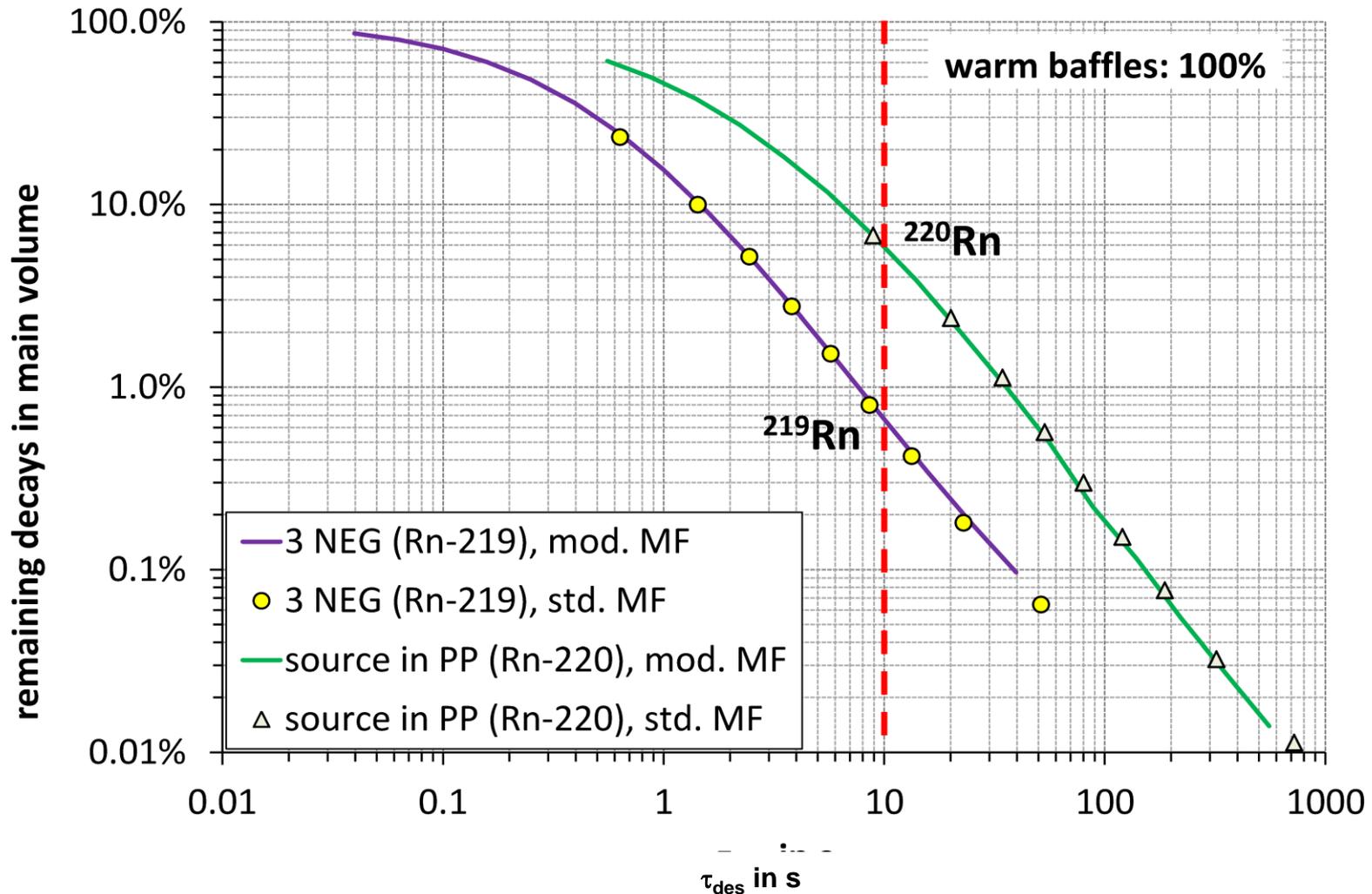
Simulation examples: baffle pumping

- reduction of Rn decays in the main volume



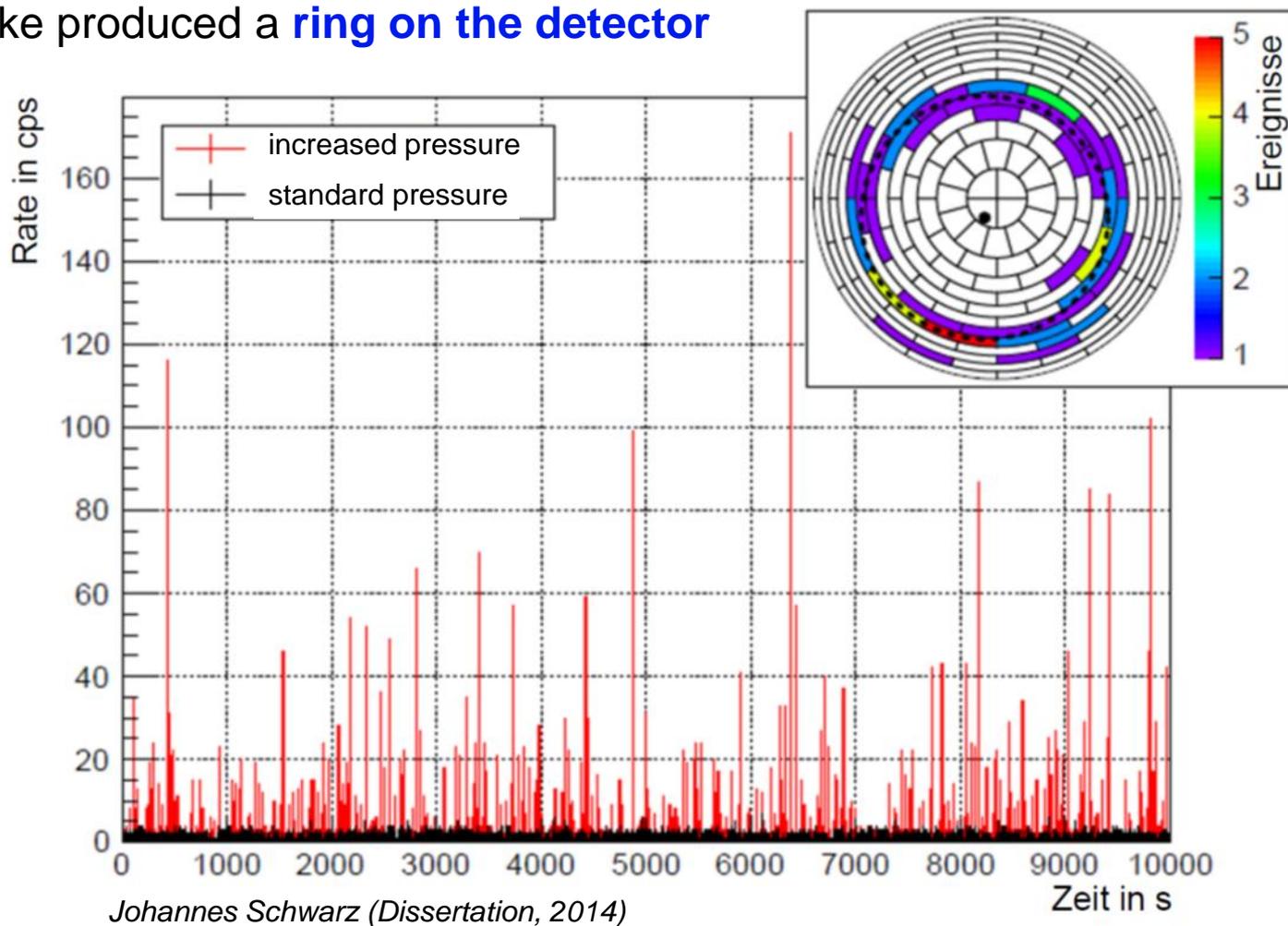
Simulation examples: baffle transmission

- reduction of Rn decays in the main volume



Measurement of Rn decays

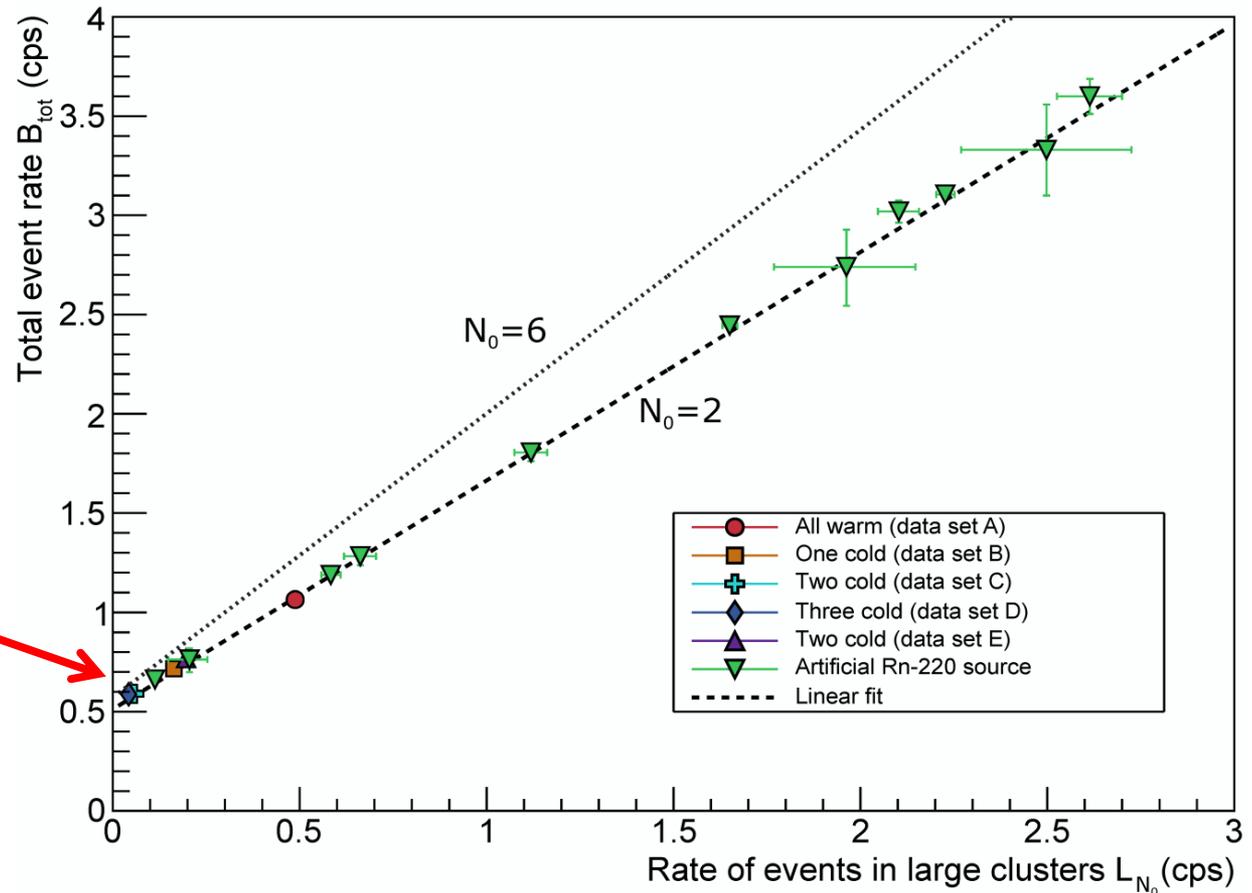
- measurement with **increased pressure** (10^{-8} mbar)
- **spikes = secondary electrons** from individual Rn decays
- each spike produced a **ring on the detector**



Radon-Induced background measurement

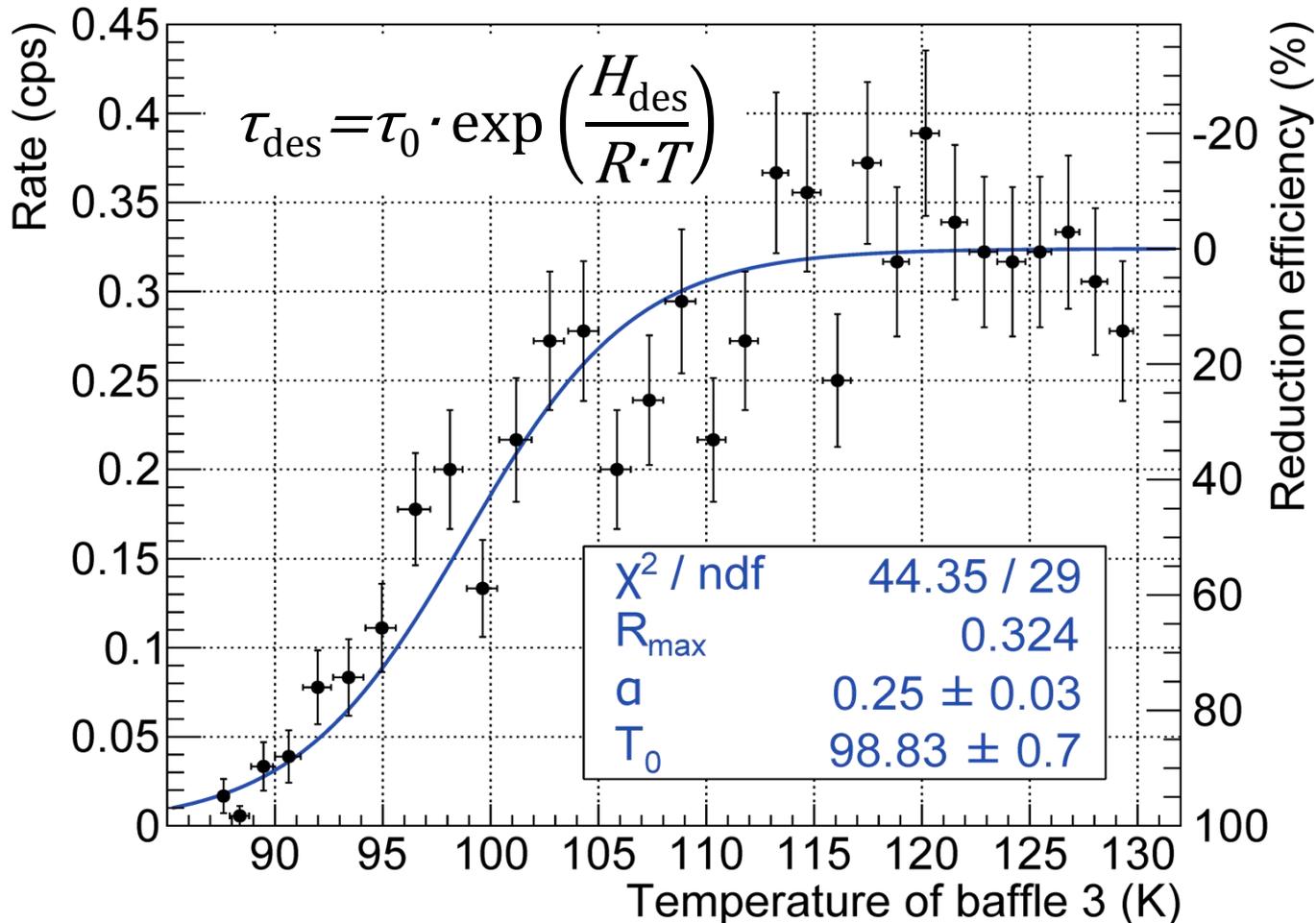
- total background with **different radon source** and **baffle temperatures**
- total event rate vs. **clustered events** (almost no accidental background)
- remaining no-radon background: **thermal ionization of Rydberg atoms**

Rydberg background
(see talk by F. Harms)



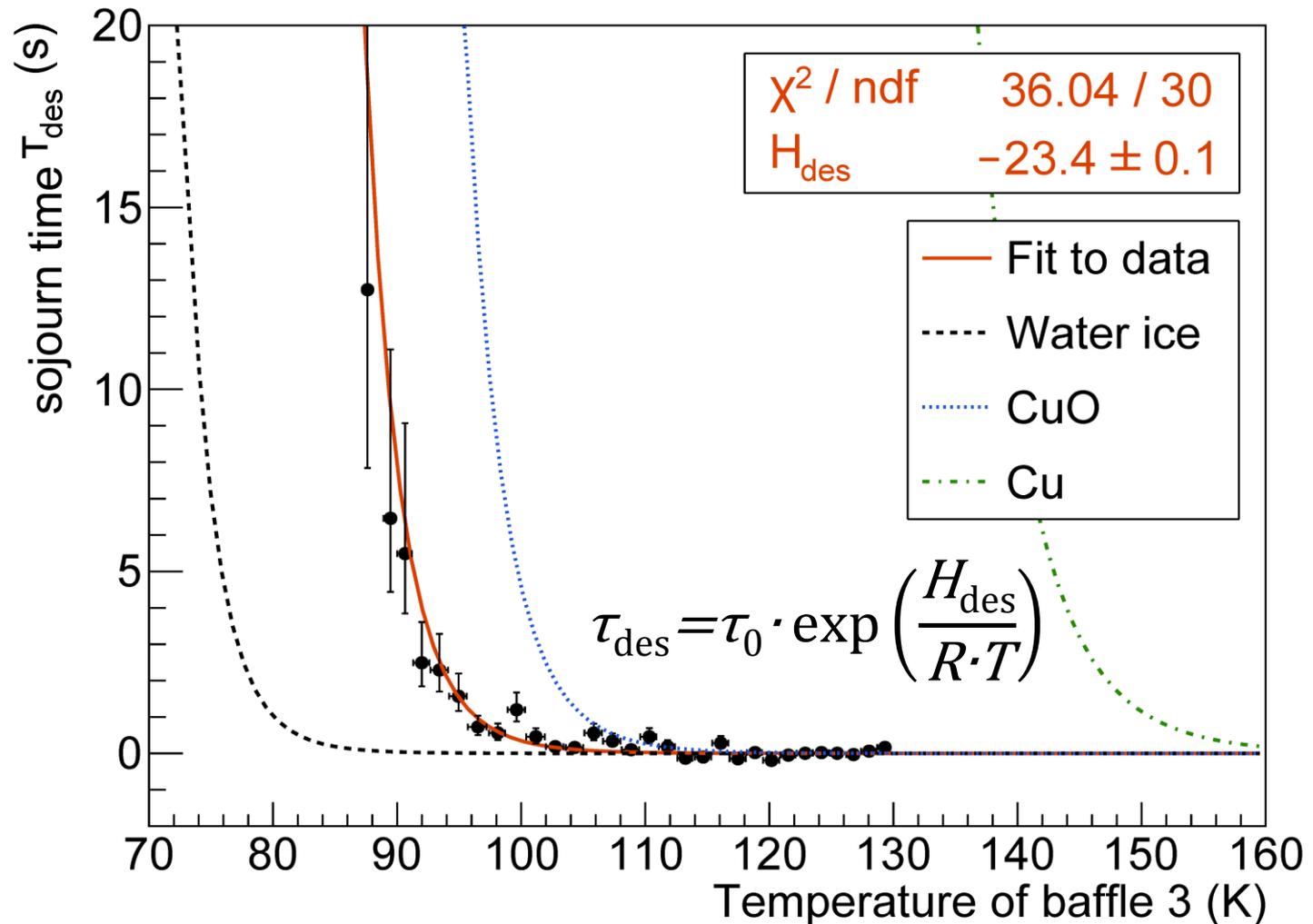
Radon-Induced background measurement

- Radon cluster event rate for different baffle temperatures.
- Reduction efficiency: 0% (warm baffle background), 100% (no radon events)



Sojourn time of cold copper cryo panels

- measurements with different baffle temperatures



Conclusions

- **Radon is a serious background in the KATRIN Main Spectrometer**
 - vacuum vessel: ^{220}Rn
 - getter pumps: ^{219}Rn
 - background rate multiplied by magnetic bottle effect (stored electrons)
- **Vacuum simulation of radioactive decay rate**
 - **calculation** of decay rates possible for simple models using „**effective sticking coefficient**“ with **standard MolFlow+**
 - **simulation** with **modified MolFlow+** source code
 - **life-time** of particles included
 - **finite sojourn time** for pumping surfaces included
 - **effective pumping speed depends on life-time** of radon isotopes
- **Radon background measurements**
 - **event cluster** vs. single event rate provides **radon related rate**
 - **cold baffles** reduce radon background **sufficiently**
 - **remaining single event background** studied (*talk by F. Harms*)

Thank you for your attention



Supported by

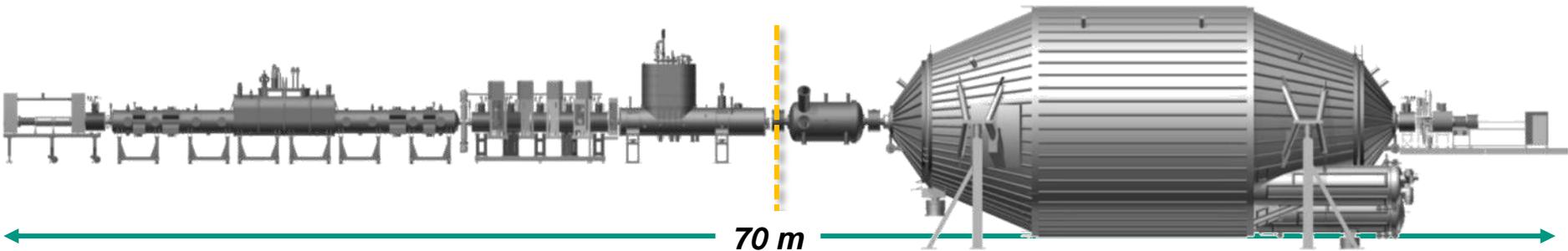


Federal Ministry
of Education
and Research

Backup slides

The Karlsruhe TRITium Neutrino Experiment

KIT
Karlsruhe Institute of Technology



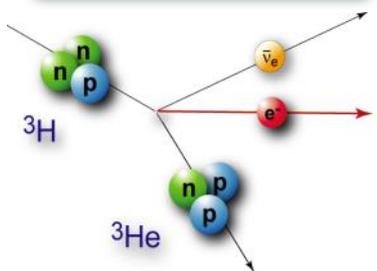
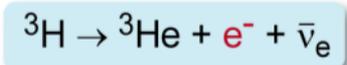
Source & Transport Section (STS)

Spectrometer & Detector Section (SDS)

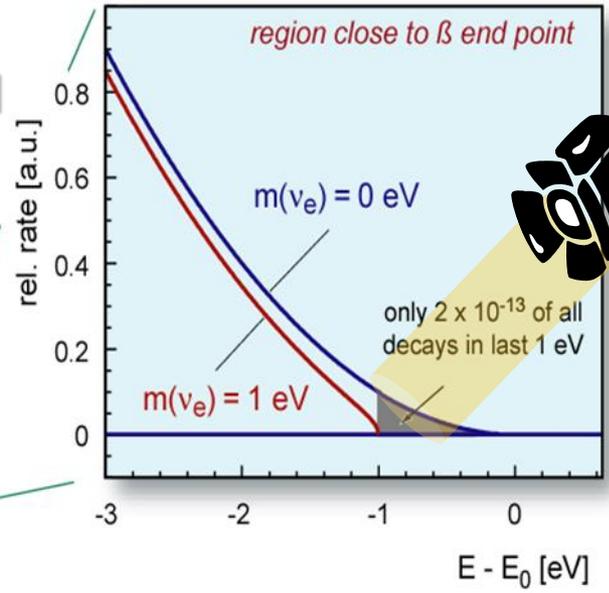
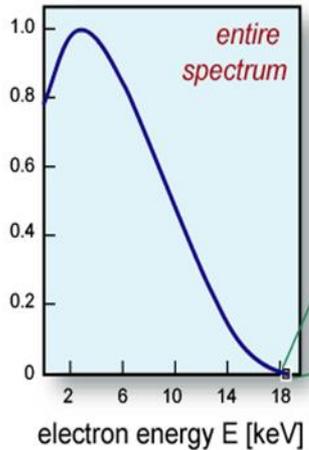
ideal β -emitter

^3H : super-allowed

E_0	18.6 keV
$t_{1/2}$	12.3 y

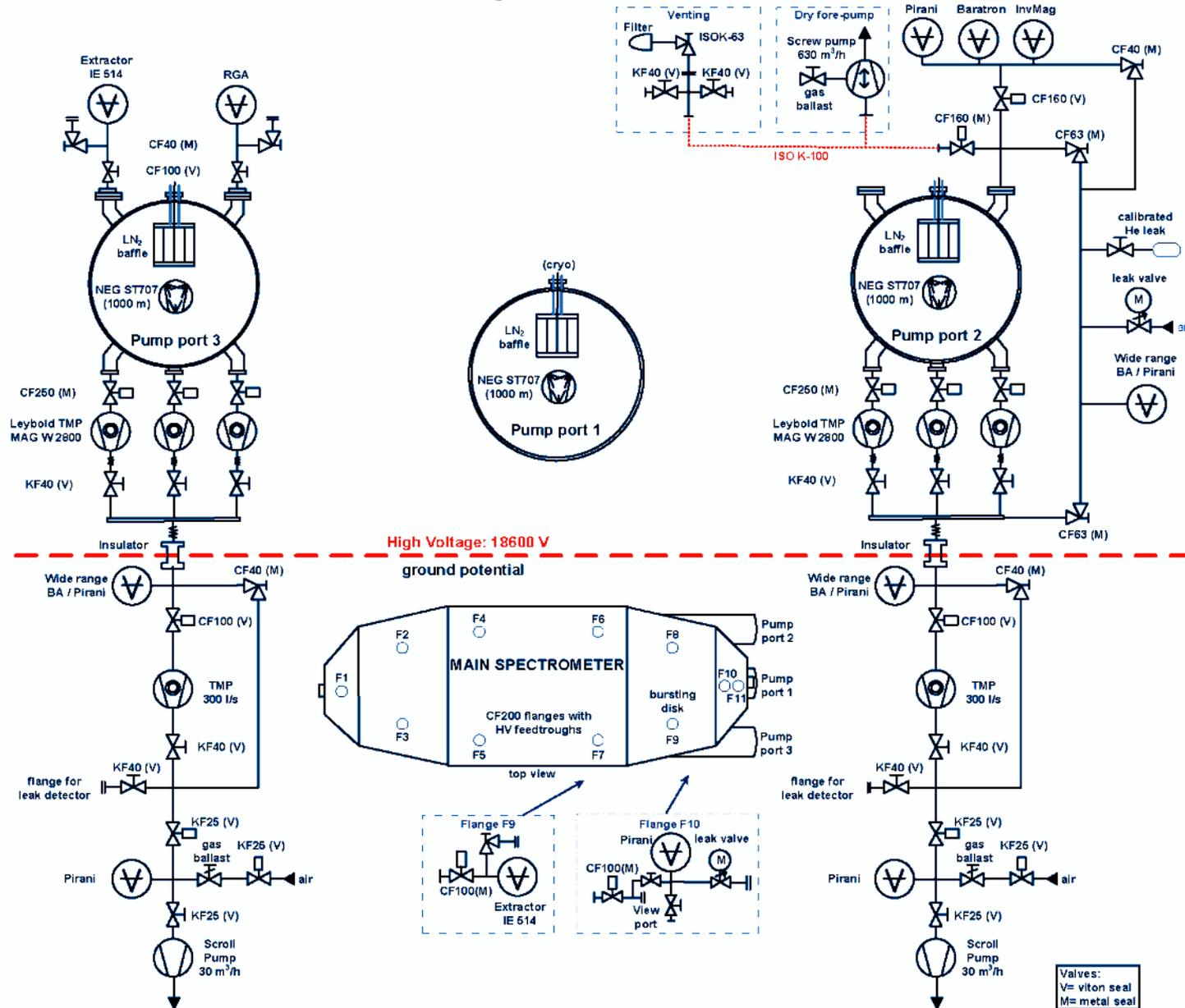


MAC-E-Filter
most sensitive method



G. Drexlin, V. Hannen, S. Mertens, C. Weinheimer, Current Direct Neutrino Mass Experiments (Review) Advances In High Energy Physics (2013) 293986

Vacuum scheme of the Main Spectrometer



KATRIN Main Spectrometer

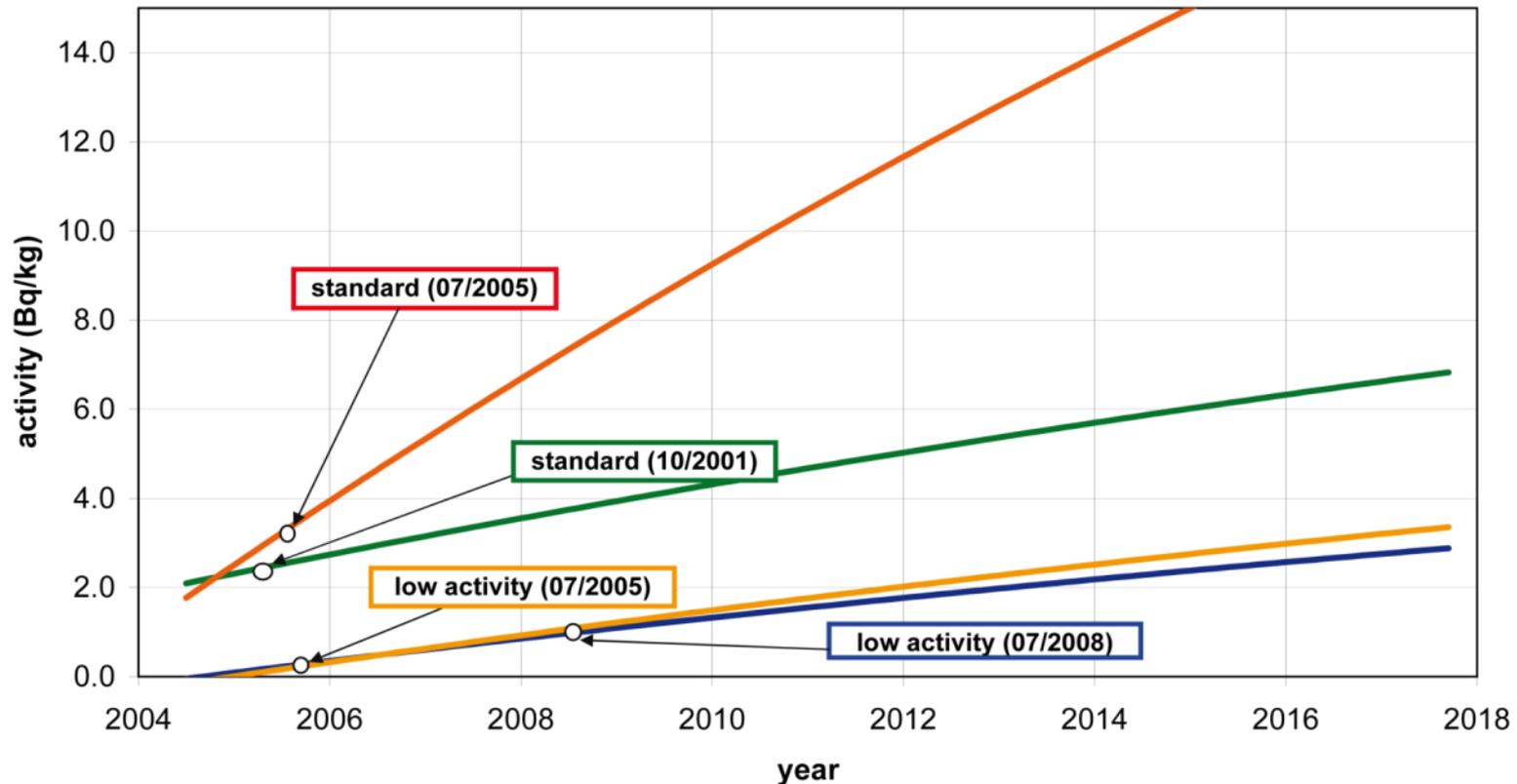
Component	Material	Temp.	Surface
Main Spectrometer vacuum vessel	316LN	20°C	690.0 m ²
Wires (23440 wires with a total length of 42400 m)	316L	20°C	33.6 m ²
Electrode frames (248 modules)	316L	20°C	436.8 m ²
Electrode rail system	316LN	20°C	58.0 m ²
Feedthrough flanges	316LN	20°C	2.0 m ²
Small components (frame NEG-pumps, etc.)	316L	20°C	1.5 m ²
Σ stainless steel	316L(N)	20°C	1221.9 m²
Σ ceramic insulators	Al₂O₃	20°C	5.8 m²
Σ anti-penning electrodes	Ti	20°C	11.0 m²
Σ ground electrodes	Al	20°C	1.3 m²
Σ surfaces at room temperature		20°C	1240 m²
Σ cryogenic baffles	Cu	77 K	31 m²
Σ NEG-strips	St707	20°C	180 m²
Volume Main Spectrometer			1240 m³

Reduction of Rn-induced background

■ Passive methods (before decay): low-activity materials

- use thorium-free **welding tips** (TIG welding)
- activity monitoring of **stainless steel**
- special batch of **SAES St 707** getter alloy

Radon-219 activity in St707 getter (KATRIN main spectrometer)



Reduction of Rn-induced background

- **Select materials** with low Rn content
- **remove Rn** from spectrometer before it decays (pumping)
- **prevent Rn from entering** spectrometer (cryo-trapping)

Rn activity in spectrometer volume

$$\frac{dN_{\text{Rn}}}{dt} = E_{\text{Rn}} - A_{\text{Rn}} - \frac{N_{\text{Rn}}}{V} \cdot S_{\text{eff}} = 0$$

$$A_{\text{Rn}} = \lambda_{\text{Rn}} \cdot N_{\text{Rn}} = E_{\text{Rn}} \frac{\lambda_{\text{Rn}}}{\lambda_{\text{Rn}} + S_{\text{eff}}/V}$$

- N_{Rn} = Rn atoms in spectrometer
 E_{Rn} = **emanation rate** (desorption)
 A_{Rn} = $N_{\text{Rn}} \cdot \lambda_{\text{Rn}}$ = **activity in spectrometer**
 $T_{1/2}$ = radioactive half-life
 λ_{Rn} = $\ln(2)/T_{1/2}$ = decay rate
 V = spectrometer volume (1240 m³)
 S_{eff} = **effective pumping speed for Rn**

Goal:

- **reduce activity by maximizing pumping speed:** $S_{\text{eff}} \gg V \cdot \lambda_{\text{Rn}}$
- $V \cdot \lambda_{\text{Rn}} = 2.6 \text{ l/s}$ for ²²²Rn
- $V \cdot \lambda_{\text{Rn}} = 15.5 \text{ m}^3/\text{s}$ for ²²⁰Rn
- $V \cdot \lambda_{\text{Rn}} = 215 \text{ m}^3/\text{s}$ for ²¹⁹Rn



²²²Rn $T_{1/2} = 3.8 \text{ d}$



²²⁰Rn $T_{1/2} = 55.6 \text{ s}$



²¹⁹Rn $T_{1/2} = 3.96 \text{ s}$



Rn adsorption on a cold surface

number of particles
in the spectrometer

$$\frac{dN}{dt} = \lambda \cdot N \qquad N(t) = N_0 \cdot e^{-\lambda t}$$

number of particles
on the baffle

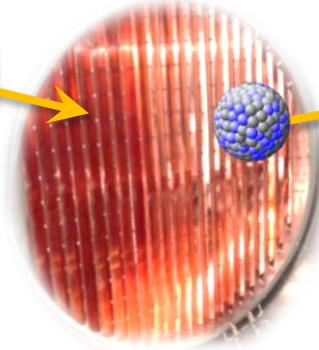
Rn adsorption

$$\lambda_{\text{ads}} = (\tau_{\text{ads}})^{-1} = S_B/V$$

$$S_B = 1/4 \cdot A_B \cdot \bar{c} \cdot \alpha$$

- S_B = pumping speed baffle
- V = spectrometer volume
- A_B = baffle area
- α = sticking coefficient (0...1)

maximise λ_{ads}



Rn desorption

$$\lambda_{\text{des}} = (\tau_{\text{des}})^{-1}$$

$$\tau_{\text{des}} = \tau_0 \cdot \exp\left(\frac{\Delta H_{\text{des}}}{R \cdot T_B}\right)$$

- ΔH_{des} = desorption enthalphy
- τ_0 = phonon osc. period
- T_B = baffle temperature
- R = molar gas constant

minimise λ_{des}

Radioactive decays

$$\lambda_{Rn} = \ln(2)/T_{1/2}$$

$\lambda_{Rn} \cdot N_{Sp}$ decays in volume: background

$\lambda_{Rn} \cdot N_B$ decays on baffles: $\lambda_{\text{des}} = 0$

Rn reduction and transmission probability

■ **reduction factor:** $R(T_1) = \frac{A(T_1)}{A(T_0)} = \frac{p(T_1)}{p(T_0)}$ with $T_0 = 293$ K

■ **pressure:** $p(T_i) = \frac{Q_{\text{NEG}}}{S_{\text{eff}}(\alpha_i) + \lambda_{\text{Rn}} \cdot V} \cdot \text{Tr}(\alpha_i)$

■ **baffle transmission:** $\text{Tr}(\alpha_i) = \frac{Q_{\text{MS}}}{Q_{\text{NEG}}} = \frac{p(T_i) \cdot S_{\text{eff}}(\alpha_i)}{Q_{\text{NEG}}} \propto \frac{\text{Hit}_g(T_i)}{\text{Des}(T_i)} \cdot S_{\text{eff}}(\alpha_i)$

(standard MolFlow: stable particles)

$$R(T_1) = \frac{\text{Hit}_g(T_1)}{\text{Hit}_g(T_0)} \cdot \frac{\text{Des}(T_0)}{\text{Des}(T_1)} \cdot \frac{S_{\text{eff}}(\alpha_1)}{S_{\text{eff}}(\alpha_0)} \cdot \frac{S_{\text{eff}}(\alpha_0) + \lambda_{\text{Rn}} \cdot V}{S_{\text{eff}}(\alpha_1) + \lambda_{\text{Rn}} \cdot V}$$

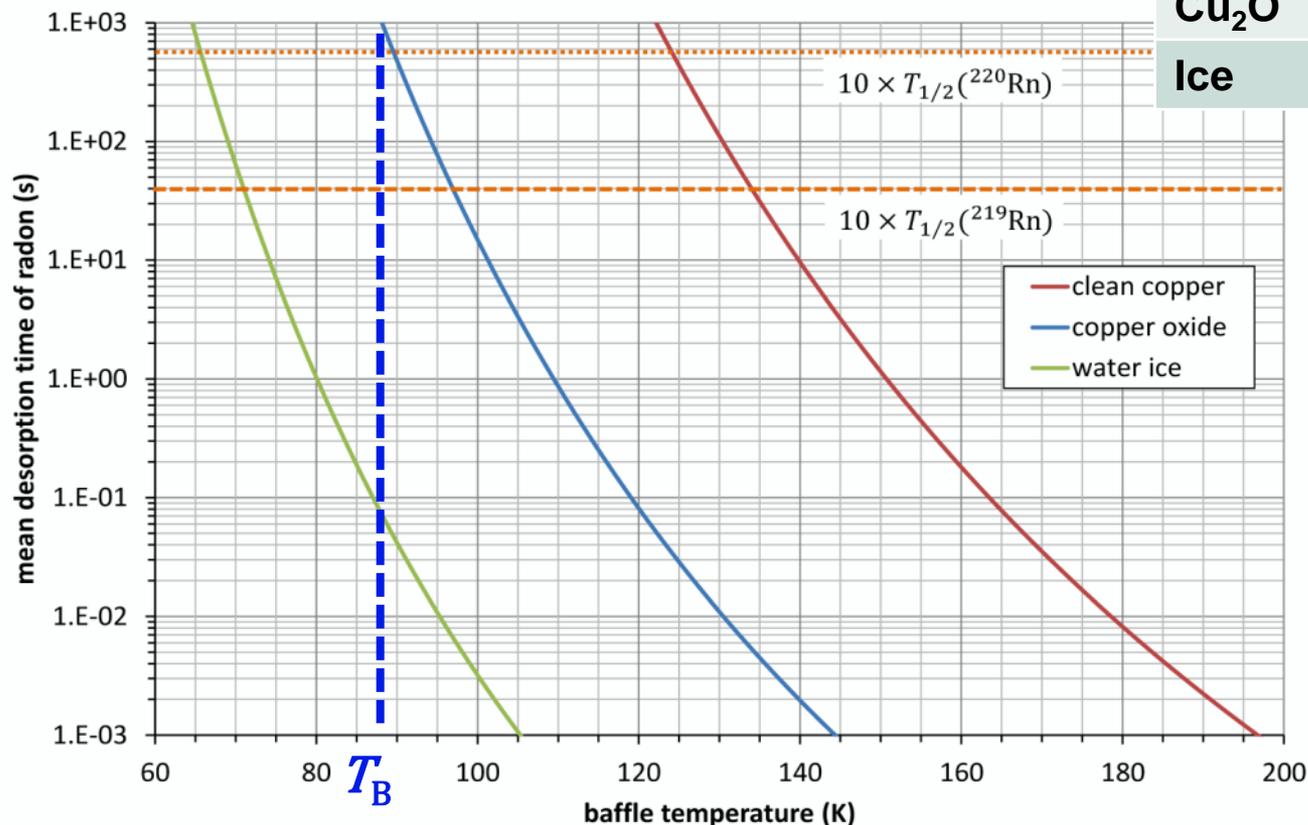
(all parameters simulated with **standard MolFlow+** and $\alpha_{\text{eff}}(T_i)$)

Desorption time of copper cryo panels

possible problem:

- water ice on cryo-panels
- strongly reduced desorption time

material	τ_0 in 10^{-13} s	H_{des} in kJ/mol
Cu	1.5 [2]	37 [4]
Cu ₂ O	3.9 [1]	26 [4]
Ice	3 [3]	19.2 [4]



[1] M. H. Manghnani et al (1974)

[2] B. Eichler et al (2000)

[3] B. Eichler et al (2000)

[4] R. Eichler et al (2002)

$$\tau_{des} = \tau_0 \cdot \exp\left(\frac{H_{des}}{R \cdot T}\right)$$

MolFlow+ simulation of radon

■ modified MolFlow+ code:

- particles can have a **mean lifetime**
- facets can have a **finite residence time**
- **sticking coefficient** usually set to $\alpha = 1$
- **absolute lifetime** (time of decay) calculated at the start of the tracking
- **decay in volume:**
 - **time of flight** in vacuum (calculated by MolFlow+) subtracted from lifetime,
 - **3D coordinates** of decay position **stored** in file,
 - **#volume_decays** incremented
- **decay on adsorbing surface:**
 - decay occurs within residence time on surface
 - **#adsorption(facet)** incremented
- **re-desorption from surface:**
 - residence time subtracted from lifetime,
 - **#hits(facet)** incremented
 - **#re-desorptions(facet)** incremented

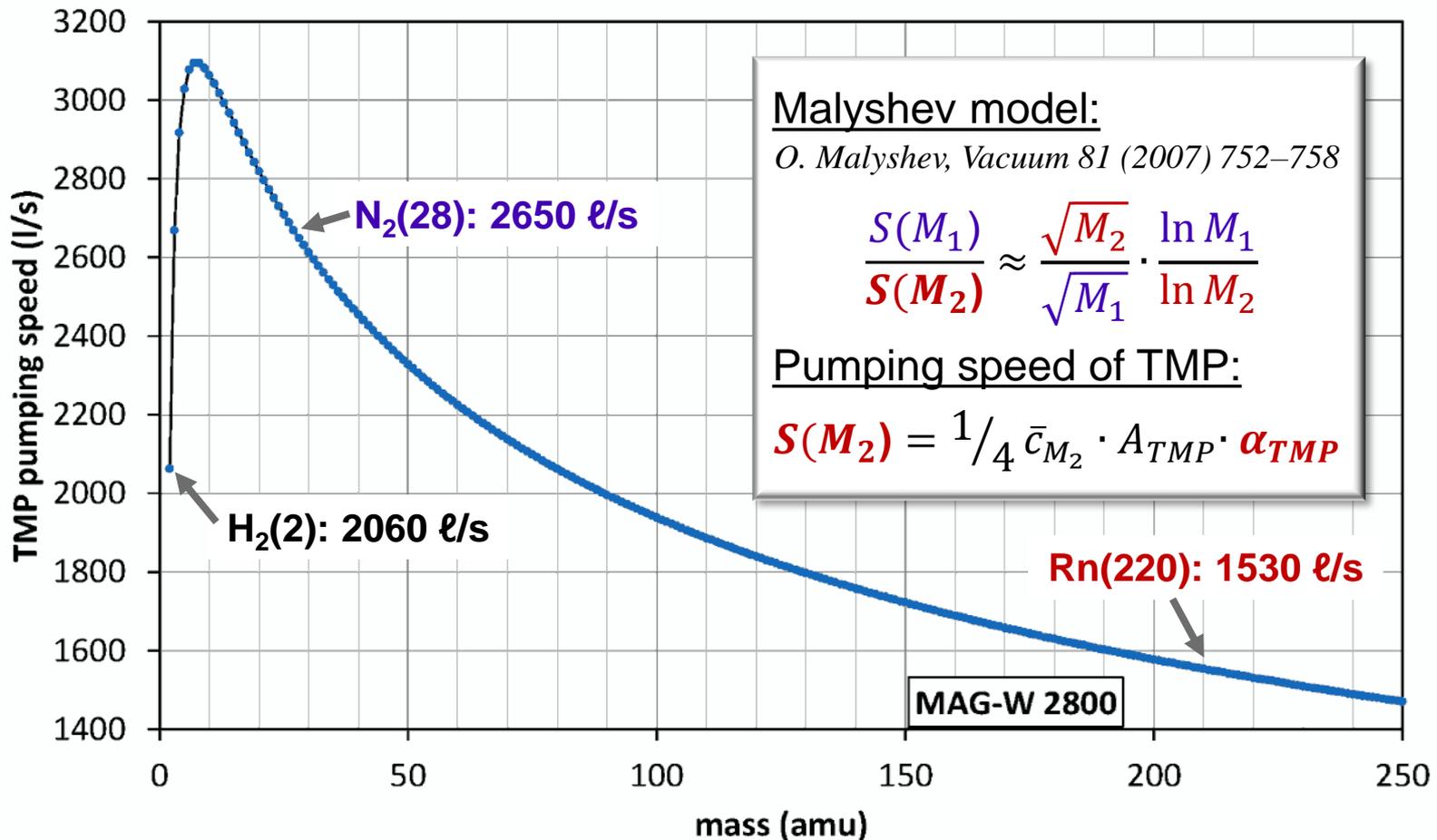
$$\tau_{\text{Rn}} = t_{1/2} / \ln(2)$$

$$\tau_{\text{des}} = \tau_0 \cdot \exp\left(\frac{\Delta H_{\text{des}}}{R \cdot T_{\text{B}}}\right) > 0$$

$$\tau_{\text{des}} = \infty \text{ if } \tau_{\text{des}} < 0$$

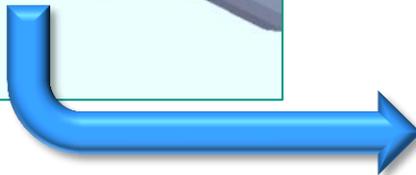
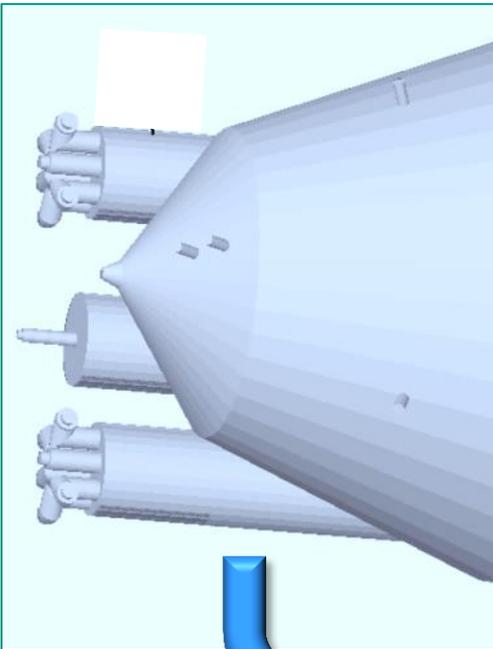
TMP simulation

- Determine pumping speed of TMP for **mass of gas particle** (Malyshev model)
- Simulate **pumping probability** $w = N_{ads}/N_{des}$
- **Effective pumping speed:** $S(M_2) = 1/4 \bar{c}_{M_2} \cdot A_{port} \cdot w$



Simulation of an effective pumping speed

- Simulate pump as surface with an **adsorption probability** α
- Determine **pumping probability**: $w = N_{ads}/N_{des}$
- Calculate the **effective pumping speed**: $S = 1/4 \bar{c}_M \cdot A_{port} \cdot w$



simplified model

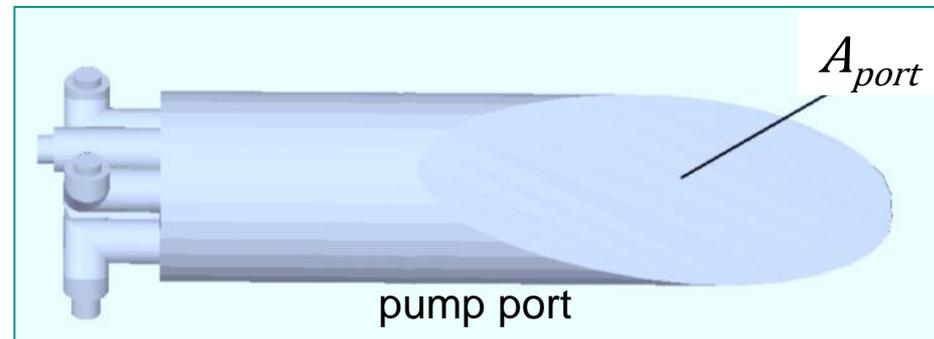
\bar{c} : mean molecular speed for mass M

$$\bar{c} = \sqrt{\frac{8k_B T}{\pi M}}$$

A_{port} : desorption area (virtual area)

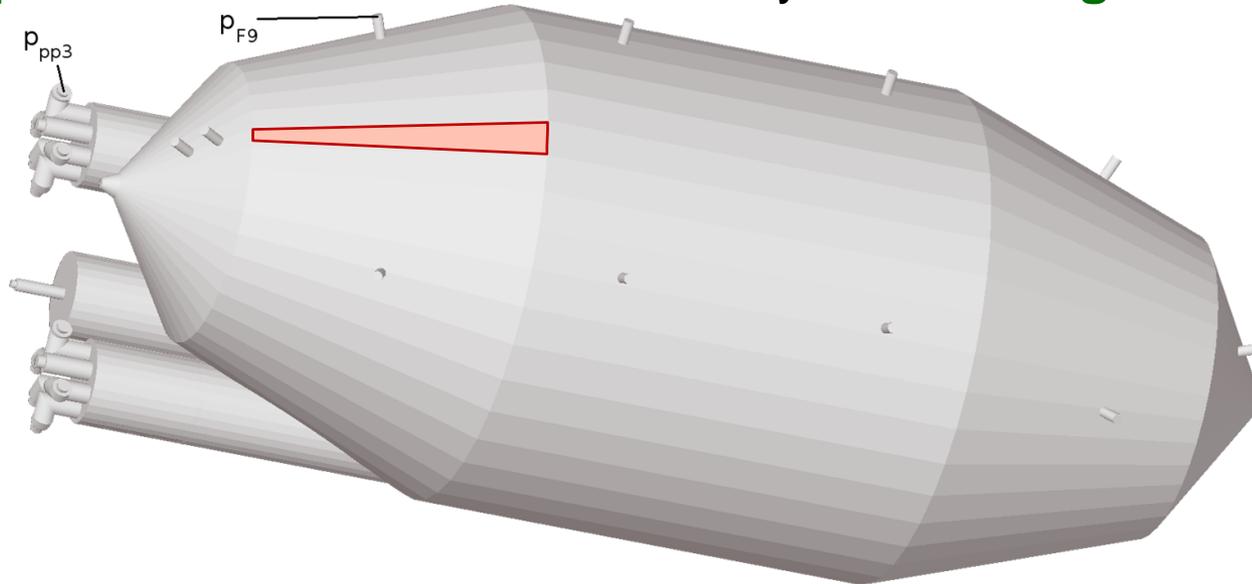
N_{ads} : number of adsorptions in pump

N_{des} : total desorption number



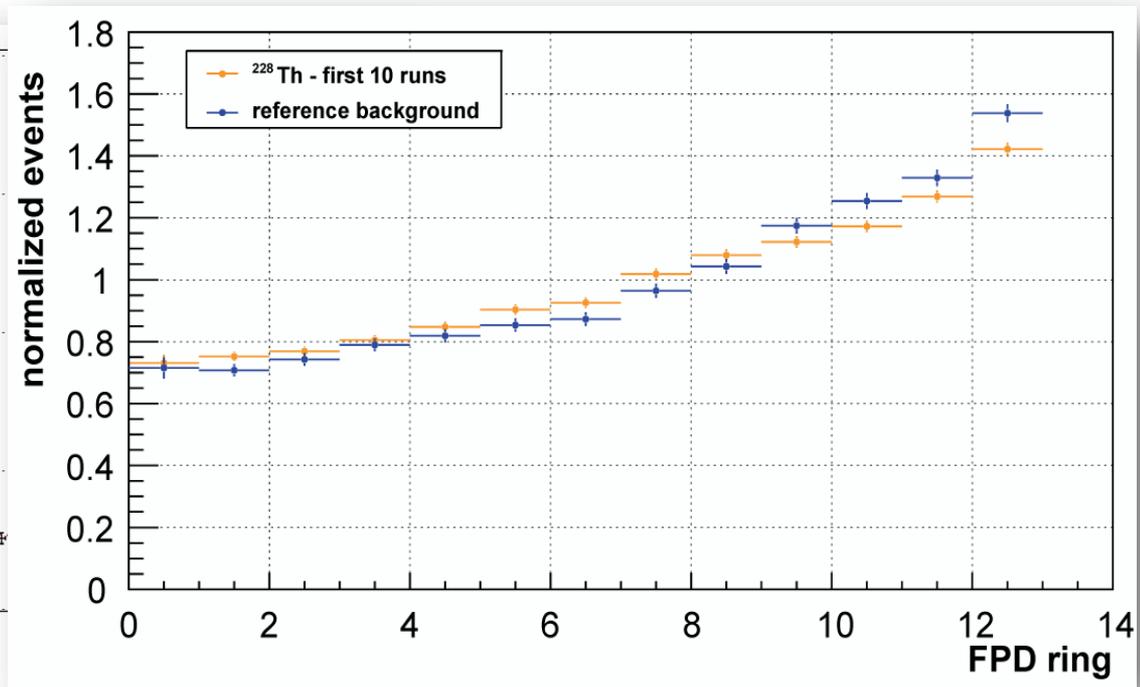
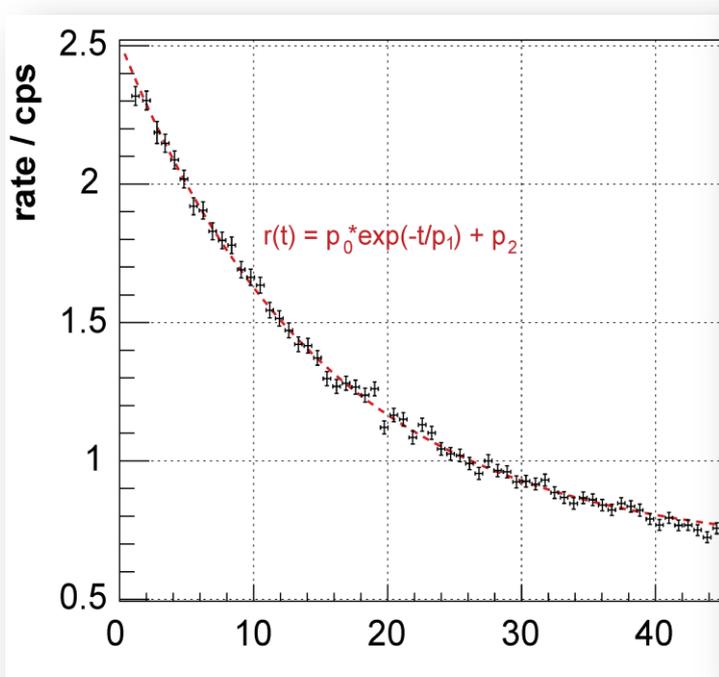
Simulation of the Main Spectrometer

- **MolFlow+**: Test Particle Monte Carlo code
- simplified model with **flat surface elements** (= *facets*)
- **particle tracked** until adsorbed (pumped out)
- each **facet** counts:
 - **#desorptions** (source)
 - **#hits** (pressure) → particle scattered or adsorbed,
 - **#adsorptions** (pumping),
- **adsorption** on a surface is controlled by the **sticking coefficient α**



KATRIN spectrometer status: Rydberg atoms

- Test of Rydberg hypothesis with ^{228}Th source (courtesy of XENON collaboration)
 - ^{220}Rn emanation (20 h exposure) \rightarrow ^{212}Pb contamination of wall ($T_{1/2} = 10.6$ h)
 - increased background rate
- after separation of source: exponential decay of rate ($T_{1/2} = 10.5$ h)
- radial rate distribution same as Rydberg background
- **Conclusion: ^{210}Pb from ^{222}Rn decays most likely cause of increased background rate**



Sensitivity and background

- Further **background reduction** measures being studied
- In addition: **several mitigation strategies** currently under investigation:
 - optimized scanning
 - range of spectral analysis
 - flux tube compression by increasing B

